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FATIGUE LIFE AND FRACTURE ANALYSES FOR THE M185/M284 BREECH RING			AMCMS No. 6126.24.H180.0 PRON No. LT3A3FUS1ABJ		
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Fracture mechanics and fatigue life analyses were performed for M185/M284 breech rings, with emphasis on ring Serial No. 1659, which failed during safe life testing after 109 pressure cycles. Mechanical and fracture properties from the breech rings were measured and used to perform yield-before-break fracture analysis. Scanning electron fractography was used to determine the size of defect present in ring Serial No. 1659 prior to laboratory testing and the types of cracking that occurred during laboratory testing. Mean fatigue life calculations were prepared for various sizes of defect and applied pressures, including the defect size measured from fractography, the pressure of the laboratory test, and the pressure of the rounds that are fired with this type of breech ring.					
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EDACTURE MECHANICS ANALYSIS OF THE C76A1 PENETRATOR AM		AMCMS No. 6126.24.H180.0 PRON No. F14XCCF6M11A			
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Fracture mechanics testing and analysis were performed for the long rod penetrator of the 105-mm C76A1 kinetic energy round. Material property and inspection results from the manufacturer of the tungsten alloy penetrator were reviewed. Fracture toughness was measured and bend energy-to-failure tests were performed from each of the five production lots for the penetrator. Analysis of the manufacturer's results and the U.S. Army Armament Research, Development, and Engineering Center's test results failed to identify any defect in the material or manufacturing process that could cause a failure of the type that occurred with one round during firing tests. A penetrator was fatigue tested so as to produce a 1.6-mm deep crack in the root of its rearmost groove. The bend energy-to-failure of					
this cracked penetrator was measure	ed to be about one-eighth of that of	an uncracked penetrator.			
Results of the tests and analyses indicate that a crack of about the same size as that in the fatigue test had been present in the penetrator that failed in firing tests. A recommendation was given to use an eddy-current inspection method in future manufacturing of this type of tungsten alloy penetrator.					
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(SPCV) measurements is preselight whose photon energy except thus SPCV measurements do not the SPCV is measured as a function of the spectrum is associated with the with experimental results perform the proposed technique is considered.	ented. SPCV measures the chan- eeds the band gap energy of the so of require the fabrication of metal ction of the energy of a sub-band a density of surface states. A quali- formed on gallium arsenide sample	ge in the surface electrical emiconductor sample. The contacts. In photo-charge gap monochromatic steady tative analysis of the propo- is passivated with a thin zing an be used as an in-line	s using surface photo-charge voltage charge induced by a chopped laser is charge is measured capacitatively, voltage spectroscopy measurements, state illumination, and its derivative sed measurement is presented along a selenide film of variable thickness, nondestructive characterization of
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FRACTURE TOUGHNESS ASSESSMENT OF PRESENT AND FUTURE PRESSURE VESSEL MATERIALS BASED ON CHARPY IMPACT ENERGY AND YIELD STRENGTH			AMCMS No. 6111.02.H611.1 PRON No. 1A11Z1CANMBJ	
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Edward Troiano and Gregory Vigila				
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Several medium and high strength at alloy steel, have been heat treated to Charpy impact energy. The correlat Underwood suggests that for A723 limitation of their study was that temperature. This study evaluates of utilizing these correlations. Results at room temperature, and tends to utilize the correlations one instance, was a conservative estimated.	lloys, including AF1410, Inconel 7 to various strength and toughness let ions investigated included those by steel, the Rolfe-Novak correlation the Charpy impact energy was much arpy impact energy and toughnes of this study indicate that the Rolanderpredict the measured fracture mate of the measured fracture toughts recommended that if a correlation	vels and evaluated for con Rolfe-Novak and Ault-W n predicts the fracture to easured at -40°F, whereas is at both room temperature fe-Novak correlation over toughness at -40°F. The hness of the material at both is necessary for estimating	steel, and ASTM A723 high strength low relations between fracture toughness and ald-Bertolo. Previous work by Kapp and alghness reasonably well. One potential is the toughness was evaluated at room re and at -40°F and considers both when predicts the measured fracture toughness Ault-Wald-Bertolo correlation, in all but th room temperature and -40°F. Utilizing ig the toughness of any of these materials,	
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treatments and resulting residu different depths and surface v notch root surface value of co both the deepest and the high life agreed well with measure growth properties of the mat magnitude of the residual stree life plot, where the ΔK is for a relationship between ΔK and	rmed with notched bend specimulal stress: shot peening, hole swaging values of residual stress near the recompressive residual stress. The holest surface value residual stress coments. The calculations account erial; the shallow surface-crack exist distribution. A consistent description of the shallow crack near the notch root fatigue life agreed well with the residual that fatigue life predictions of	ng, and tensile overload. The thronotch root and different fatigue lighest life was measured from or distribution. Fracture mechanicated for the following factors that on figuration; the applied loading ription of fatigue life was obtained and in the region of compressive sults from both the untreated no	the treatments produced widely lives depending mainly on the verload specimens, which had s-based calculations of fatigue t affect fatigue life: the crack g; and the depth and surface d from a ΔK versus calculated the residual stress. A power-law teches and those with the three
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surface can be defined by the get r, r', r'', r_o , and r_o is derived. The gauge surface by a filament winding matrix r_o is the filament winding matrix.	on for a surface of revolution neralized Clairaut relation rSinglobal satisfaction of this inequichine. If the surface is concated guaranteed. By "windable" we the wound filament does no	$mw = r_o$, where w is the mendion uality guarantees the windabilitive anywhere $(r'>0)$ and a more mean that the winding data put bridge. In addition to this negative	
14. SUBJECT TERMS Filament Winding, Geodesics, 1	Differential Geometry, Surface	e of Revolution	15. NUMBER OF PAGES 21 16. PRICE CODE
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Samuel Sopok and Jay Hoessle			
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14. SUBJECT TERMS Chemical Analysis, Gun Steel, Optimize	ed Emission Spectroscopy		15. NUMBER OF PAGES 28 16. PRICE CODE
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the trajectory of the projectile increases projectile velocity, the deflections during firing are re- is necessary to establish a mo- minimize muzzle deflection.	e. As the propellant temperature hus affecting range, accuracy, and elated to projectile velocities, white are accurate estimate of the prop	e varies, its burn rate also var d penetrating capability for ki ich in turn relate to the prope bellant temperature at the tim approach that can be used to	e dynamics of a cannon and thus ies. A faster burning propellant netic energy projectiles. Muzzle llant temperature. Therefore, it e of ignition to account for and develop an emulator design. An
14. SUBJECT TERMS Thermal Emulator, Temperati	ure Gage	·	15. NUMBER OF PAGES 11 16. PRICE CODE
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test and analysis procedures. Notche two carbon fiber/epoxy materials, a rei 2-mm and 4-mm; and three specimen specimen with arm height-to-specimes specimen, including those for stress in and for a/W in terms of V. Relations specimen were also derived.	d specimens were tested on latively brittle T300 fiber/976 configurations, the standard n width ratio of 1.9. Stress atensity factor, K, and crack-hips for the bending stresses	two types of symmetrics 5 epoxy and a tougher AS three-point bend and con and displacement expres mouth opening displacen that control self-similar s	of developing translaminar fracture toughness al layups, quasi-isotropic [0/45/90] and [0/90]; 4 fiber/977-2 epoxy; two laminate thicknesses, appact configurations, and an extended compact sions were obtained for the extended compact ment, V, in terms of relative notch length, a/W, and off-axis cracking for the extended compact
damage in the bend specimen. Two to the notch in predominantly 0° fiber K at maximum load, K _{max} , determined as a measure of fracture toughness.	types of notch-tip damage w layups, and that which occur in a way that took account For deviations from the This criterion also excluded	were characterized using to shead of the notch in queen of the effective crack grainear P-V plot correspondents with damage of the	he standard compact specimen and load-point radiography, that which extends perpendicular uasi-isotropic and 90° fiber layups. The applied owth up to the maximum load point, was used ording to $\Delta a/W \leq 0.04$, K_{max} gave consistent type that violates the basic concept of fractures. Plots of K_{max} versus $\Delta a/W$ showed increasing

14. SUBJECT TERMS

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resistance to crack growth for quasi-isotropic layups and constant resistance to crack growth for predominantly 90° fiber layups.

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weaponry is extremely accurate can should embrace the minds zero' concept brought about be entire fleet using only a few the determined. Therefore, for the that contributes to accuracy) man a comprehensive study into the their effect upon dynamics at the in the early 1990s. Modelling the overall goal is to provide a jump offset for a specific round randomly drawn from an expect of output responses having its distribution. For the test data elliptical method of shot impact of gaining improved accuracy as	e, we should not embrace the meet that the best in tank gun accurate the downsizing trend in today tanks and gun tubes. The confector to work, variability in the concept to work, variability in the relationship among the character relationship among the character muzzle and shot accuracy. This performed using Benét's gun aiming point correction factors to and ballistic load. In this type sted statistical distribution. There is own characteristics. The like used and the analysis run, fifty	indset that the best in tank guracy has been achieved. We racy has been achieved. We r's army means that zeroing tribution of individual tubes a tube-to-tube manufacture (for through the use of computeristics of gun tubes, project he data is provided from the vibration model and a recerbased upon system dynamics of analysis, the values of undefore, a given distribution of lihood that a response occur percent of the samples shoulding more rounds and gun tu	ues. Even though our mechanized in accuracy has been achieved. We can and should do more! The 'fleet exercises will be conducted for the sto a tank's accuracy is no longer (or more importantly the variability ter simulation. This report presents tiles, gun mounts, and ballistics and dynamic index tube test conducted only purchased gun vibrations code, and an empirically determined exit certain or unknown parameters are input values results in a distribution its is cast in terms of a probability we promise for the use of this semibes is recommended with the intent
14. SUBJECT TERMS Gun Dynamics, M1A1, Tank (Probabilistic Analysis, M256 Te	Gun Accuracy, Modal Analysis, ank Cannon, Kinetic Energy Pr		15. NUMBER OF PAGES 94 16. PRICE CODE
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6. AUTHOR(5) John H. Underwood, Anthony P. Pa at Newcastle, UK), Daniel J. Corrig	rker (University of Northumbran, and Michael J. Audino	ia		_
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Sections of camon tubes with inner fatigue failure occurred. The failur purpose of evacuating combustion including 0, 30, 50, and 100 percent hole and the measured fatigue life, wall position and significantly increased reacturations gave a good description concentration of the hole, crack significant the crack surfaces. As with measure the ratio of outer-to-inner radius of fatigue life. 14. SUBJECT TERMS Fatigue Life, Thick-Wall Cylinder	er radius of 53, 60, and 78 mm re locations were along 2-mm re gases from the cannon after first. The amount of overstrain aff. Increasing the amount of overseased fatigue life. The amount of overstrain aff. Increasing the amount of overseased fatigue life. The amount of overstrain aff. Increasing the amount of overseased fatigue life. The amount of overstrain aff. Increasing the amount of overseased fatigue life, taking accept and shape, material fatigue red fatigue life, the calculated in the tube and the presence of particular and the pa	noles cut through the came ing. The camons had var fected both the initiation postrain moved the crack initiation sigue life were performed count of tube configuration crack rate behavior and y life was significantly affect ressure in the evacuator ho	ious amounts of autosition of the fatigue iation from the tube for comparison with, applied pressure, a ield strength, and poted by the amount le also had substantial.	ofrettage by overstraining, a crack along the evacuator inner radius toward a mid- th the measured lives. The amount of overstrain, stress ressure in the hole and on of autofrettage of the tube.
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technology was developed to detect sensor data and activates a remote t seizure activity, therefore, false als differentiating seizure activity from	the minor, barely perceptible treme etherless alarm when a seizure is de arms do occur. Neural networks has a casual motion. The network uses	ors characteristic of partial seize stected. However, the sensor re ave been studied as a means of elements of the normalized po-	reizures in children. A unique sensor ures. A microcontroller analyzes the esponse is similar for both casual and if analyzing the sensor response and wer spectrum of the response data as by detecting seizures than the method
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modules by straightforward tra	tensor analysis, such as Christo inscription of their defining equat	fell symbols and curvature tensorions. The built-in functions can thatica formulation is illustrated by	nen be used to perform tensor
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than 26 psig, and the coefficient	drops our rapidly at press	and to hot the property of		res greater
than 26 psig, and the coefficient 14. SUBJECT TERMS 155-mm Self-Propelled Howitzer	, Gas Dynamics, Model B	Bore Evacuator Performs	ance, 15. NUMBER OF	res greater
14. SUBJECT TERMS 155-mm Self-Propelled Howitzer Staggered Ejector Nozzles, Shoc Discharge Coefficient, Mass Flor	r, Gas Dynamics, Model B k Tube, Reservoir Charge w Augmentation Ratio, Vo	Bore Evacuator Performs	ance, 15. NUMBER OF	res greater
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elastic strains that develop as a rest cases. They show that a significan depending on the lay-up and cure cy Several possible solutions are prese:	ult of gun barrel manufacture a tresidual stress state will exist cle, large localized stresses car nted. A simple technique for n cension levels up to 7 pounds v	and field use is presented. Not because of the filament wing be generated which could coneasuring the tension during were employed successfully	erformed. A technique for calculating the fumerical results were obtained for several nding processing technique. Furthermore, ause defects such as longitudinal wrinkles. filament winding was developed and used in the experiments. The use of such high
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welds, and the other addressing the fifracture. These fatigue and fracture m Army Armament Research, Developm investigations. A brief general summ structures. Specific fatigue crack initia box beam of a cannon carriage. Re	nal fracture of the welded con ethods will be described by ref- ent, and Engineering Center, ary will be given of fatigue a tion tests and analysis methods event improvements and simp	mponent and the fracture erring to recent work from primarily fracture case stu and fracture methods and will be presented, using en lifications in J-integral fr	toughness tests used to characterize final a the technical literature and from the U.S. ady and fracture test method development concepts that have application to welded tample results from a welded stainless steel acture toughness tests will be described, weld metals and heat treatments will also
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of fracturefast fracture, fatigu tests and related analyses that l and carbon/epoxy laminates.	dly applied to failure of armamer e cracking, and environmentally-a nave been useful to characterize fr	ssisted cracking. This rep acture in armament comp te toughness, notch fatig	ed by each of the three general types out describes some fracture mechanics onents made from high strength steels ue life, and environmentally-assisted nates.
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A TITLE AND SUBTITLE NONDESTRUCTIVE EVALUATION OF SPUTTER-DEPOSITED TANTALUM CARBIDE REFRACTORY COATINGS S. Lee, W.J. Heffeman, J. Walden 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benét Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050 9. SPONSORING MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Close Combat Armaments Center Preatinny Amenal, NJ 07806-5000 11. SUPPLEMENTARY NOTES Presented at the Sixth International Conference on Nondestructive Characterization of Materials, Oahu, Hawaii, 7-11 July 1 Published in the Conference Proceedings. 12a DISTRIBUTION AVAILABILITY STATEMENT Approved for public release; distribution unlimited 13. ABSTRACT (Maximum 200 words) Desirable characteristics of refractory coatings for future projectile launchers include high wear resistance, high melting phardness, electrical conductivity, good adhesion, thermal stability, and high plasma resistance properties. Sputtered tant and stantalum compounds, such as tantalum miride and intalianum carbide are being considered as future coatings to endurn high pressure, high temperature, and aggressive chemical environment of the bore. In this work, tantalum and tantalum arbide are being considered as future coating to endurn high pressure, high temperature, and aggressive chemical environment of the bore. In this work, tantalum and tantalum carbide was deposited at methane concentrations above 25 percent, and a mixture of inantalum carbide was deposited at methane concentrations above 25 percent, and a mixture of inantalum and tantalum carbide was deposited at methane concentrations of the representation confined and tantalum carbide and exposition rate, Knoop hardness, and temperature coefficient of resistivity are sensitive function of percentage methane concentration. Coating composition, crystalline structure, passize, preferred orientations, deposition rate, Knoop hardness, and temperature coefficient of resistivity are sensitive function of percentage methane concentration. Co	1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE	3. REPORT TYPE AND D	ATES COVERED
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contraction chromium were plated of	nto samples of 4340 grade steel at x 10 ¹⁵ to 3.1 x 10 ¹⁸ atoms/cm ² an noop microhardness, and pin-on-d	nd subsequently implanted with the implantations were con	tudied. Both hard chromium and low with N ₂ ⁺ or Ar ⁺ at atom energies of 75 inducted at both room temperature and a study the effects of ion implantation	
properties improved with an increase in the coefficient of friction and a m with nitrogen at elevated temperature at the same condition. The elevated	ing nitrogen dose. For both kinds of the seasurable decrease in the wear rate of the showed improved friction and we temperature implantations also appose the hardness was increased three of the contraction chromium. At the h	of chromium, the nitrogen im b. At the intermediate doses car properties compared to the cared to decrease the hardness times that of the unimplanted highest dose tested, the max	neral, the hardness, wear, and friction aplantation resulted in a 50% reduction tested, some of the samples implanted a room temperature samples implanted as of the bulk chromium. For the room I hard chromium and slightly less than imum nitrogen concentration reached	
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Two types of ASTM A723 steels I	save been investigated fo	r their low	cycle fatigue behavior (l	ess than 10	cycles to failure). Specimens
were tested in four-point bending, Neuber notch analysis (classic and	d elastic/plastic remote (otches, and	the measured fatigue live	es were con	mpared with those predicted by
Comparison of measured and pred	icted lives indicates that	the elastic	plastic Neuber analysis	underpredic	ets the measured fatigue life by
as much as 67 percent at large stra	ins, and becomes a bette	r predictor	of life as the applied stra	ins decreas	se. The elastic Neuber analysis
also underpredicts the measured fa	tigue lives by 45 percent	t at large a	pplied strains, but seems	to accurate	ely predict lives at reversals-to-
failure greater than 100. The fraction over the full range of strains inves		assumes e	elastic stresses at the crac	k tip, and p	predicts lives within 30 percent
The results show that the Neuber	notch englysis is not as	anad an in	diame of the law such	fatiana hai	haniar of A700 at 1 1 1 1
fracture mechanics life prediction to	echnique. As the life eve	les-to-failt	ancaior of the low cycle are decreases, the Neuber	analysis po	edicts lives that are two to three
times more conservative than those	experimentally measure	d. Since t	he fracture mechanics app	roach and	the elastic Neuber approach are
fully elastic stress-based, one can o	conclude that for this class	ss of steels	, an elastic-based life pre-	dictions tec	hnique works even through we
are believed to be in a plastically-	iominated regime.				
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This work describes a response the established at the New York Sevaluate the remaining safe live commercial off-the-shelf ultrasory of the 25DL precision thickness.	o the need for a practical non-diate Department of Transporta es of the culverts. The technical requipment and piezoelectric gage and the B120 bubbler with the pump to provide continuous	tion. The proposed method value developed uses the ultrastransducers in a bubbler configuration of the configurati	onic pulse-echo technique with uration. The equipment consists
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A systematic study of the rate applied to Euclidean point set required for 5 percent converg for the fractal sets studied is Approximately 25 times as ma algorithm employed in the pro-	e of converge s, Koch consi gence of the b determined any points are	tructions, and a symmetric counting (for 0 ≤ by the generalized a required for 1 percentages)	netric chaotic mappin q ≤ 25) and correlation dimension D(q) and tent convergence. The	g is describe on integral (is given by e box-based	cd. The number of points N_5 (for -25 \leq q \leq 25) algorithms $\log_{10}(N_5) \approx 2.54$ D(q)-0.11. I correlation integral (BBCI)
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diameter to tensile at the outside treated previously. In order to measured as a function of radial load to indent the sample surfatechniques. From a model proposed plastic deformation was derived as we saw that the effect of reside formation: plastic deformation is enhanced for a tensile residulis detectable for the tests using (i.e., less total plastic deformation hardness dependence on residulations.)	all of a hollow steel cylinder the diameter. The question of less generalize the previously deal position using various hardness to measure its hardness. So seed by Frankel, Abbate, and red, and the experimental depictual stress on measured has all stress, therefore the measure larger loads, R_c and Rockwell on). The Rockwell-A (R_A) and all stress. We point out that (at residual stress can affect the	eveloped concepts, in this ess testers. Each of the hard the residual stress of the Scholz, the relationship be endence of R _C on residual runess stems from the effect as the form a compressive red hardness is decreased. I-D (R _D), and becomes was the Microdur testers us to Rockwell-C and Rockwell-C and Rockwell-C and Rockwell-C and Rockwell-C.	I varies from compressive at the inside hardness varies with residual stress was report the hardness in the wall was ardness testers used a different applied sample was measured using ultrasonic tween the residual stress and the onset stress was shown. From previous work fect of stress on the onset of plastic residual stress, and plastic deformation From this work, we see that the effect shed out for the tests using lower loads sing Vickers indenters did not show the cill-D hardness tests on gun steel should ockwell-C and Rockwell-D tests can be
14 SUBJECT TERMS Residual Stress, Hardness, Plan	stic Deformation, Yield Crite	ria, Ultrasonic Inspection	15. NUMBER OF PAGES 28
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Stuart Dunn*, Samuel Sopok, Dou	vales C	*oute#	-		
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				ing code provides the necessary missing	
				e analysis and design information that is	
unattainable by experiment alone.	At the	current stage of code develop	ment, single-shot compari	isons can be made of either the same gun	
				ex computer analysis is based on rigorous	
				nd rocket nozzle community over the last	
				analyses for chromium and gun steel wall	
				or ballistics (XNOVAKTC) and nonideal	
				or gun barrels, include the standard rocket wall material ablation conduction erosion	
				es for each material as a function of time	
				heat load axial position, predicted single-	
				million more than uncracked chromium.	
				ablation at the chromium cracks leaves	
unsupported chromium, which is s				War vinonium venogo (CGVC)	
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The metal plating industry is constantly looking for better online procedures to monitor critical process constituents and increase plating quality and efficiency. The advantages of online monitoring include direct sampling, process control, bath quality control, data processing, hazardous waste monitoring, chemical reclamation monitoring, and chemical additions. These advantages reduce costs, manpower, and downtime, and improve quality. Three new online titration procedures were developed, tested, and evaluated for the monitoring of sulfuric acid, Cr(III), and Fe(III) in chromium plating solutions. Likewise, one new online titration procedure was developed, tested, and evaluated for the monitoring of Fe(II) in electropolishing solutions. These methods were developed at Benet Laboratories and were tested at Brinkmann Instruments, Inc. (Westbury, NY). In general, these four new online procedures from above are Cr(VI) reduction then ionselective potentiometric, direct colorimetric, Cr(VI) reduction then complex-formation colorimetric, and direct redox titrations, respectively. The optimum operating tolerances of these four chemical species are 2.5 to 3.5 g/L, 0 to 7.5 g/L, 0 to 7.5 g/L, and 0 to 7.5 g/L, respectively. The first chemical constituent is purposely added, while all other constituents are unwanted low alloy steel plating process by-products. Chromium plating solutions also contain 230 to 270 g/L chromic acid. Electropolishing solutions also contain 640 to 730 g/L phosphoric acid and 795 to 895 g/L sulfuric acid. Critical low concentration chemical constituents in the chromium plating process are rapidly monitored using these online titration procedures. These new procedures nearly equal precision and bias of previous offline procedures. The precision, bias, and reliability of these new procedures should be further tested and evaluated for at least a year before adoption. These new online procedures marginally-to-adequately determine critical low concentration constituents in chromium plating process solutions.

14. SUBJECT TERMS Online Chemical Characterization,	15. NUMBER OF PAGES 23		
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J.H. Underwood, M.J. Audino, and J.	vv. 110ab	Į.	
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Calculations of the likelihood of a saft 155-mm XM297 cannon tube are deproperties of two types of ASTM A72 the evacuator and mount interface not radius. Effects of pressure, autofrett calculations. Comparisons are made similar cannon tubes. Environmental with mean life from tests, two sets of of minimum expected mean fatigue life at these locations.	escribed. Yield-before-break cal- 3 steel. The mean fatigue life cal- ches, the coolant channels, the co- age residual stress, local residual with measured mean fatigue live cracking in areas of coolant access f notches on the tube outer diame	culations are based on the fracticulations are performed for muzz solant entry ports, the thread sect atress, and notch depth and roses from recent hydraulic pressures is also assessed. Based on the ter and the coolant channels at a	the toughness and yield strength the brake and bore evacuator holes, for notches, and the chamber inner to radius are accounted for in the e safe service fatigue life tests of the calculations and comparisons midwall are identified as locations
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Traditionally, this problem is solved	by using some combination of pr inadequate for the problem at har	essure washers and especial id (the 120-mm M285 system	excessive vibration and shock loading. lly designed bolts. In the present work, n), and the problem was solved by using e of the bolt-loosening mechanism.
14. SUBJECT TERMS Bolt Loosening, Shock and Vibration Bolt Loosening Due to Shock, Bolt Is			15. NUMBER OF PAGES 12 16. PRICE CODE
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Gregory N. Vigilante and Daniel R.	Fusco		
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Four high strength materials, ASTM Gun (RLPG) Program. Experimental as part of this investigation.	A723, PH 13-8 Mo, AF 1410, and heat treatments, mechanical proper	Inconel 718, were evaluated for ty tests, and environmentally-	or the Regenerative Liquid Propellant assisted cracking tests were conducted
propellant (LP) at both ambient and	slightly elevated temperatures (175°F). The duration of test	d compact specimens in XM46 liquid ing was six months and five hours, e solution unchanged for the duration
both ambient and slightly elevated te	mperature (175°F) XM46 LP. Bec he materials tested were highly sus are tests conducted on A723 and	eause no macroscopic cracking ceptible to XM46 LP for the game an experimental heat treatmental heat heat treatmental heat treatmental heat heat heat heat heat heat heat heat	lace in any of the materials tested in took place, a valid K _{EAC} value could given test conditions. However, some ent of AF 1410 showed evidence of a XM46 LP.
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14. SUBJECT TERMS Regenerative Liquid Propellant Gun	YMA6 Liquid Propellant High 9	Strength Materials	34
Regenerative Liquid Propellant Gun Environmentally-Assisted Cracking,	Stress Corrosion Cracking, Mech	anical Properties	16. PRICE CODE
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An exploratory prototype multi-lug breech block/ring assembly was designed for future projectile launchers. The new geometry redistributes the applied load to several surfaces rather than one surface in conventional breech to react the load. Induced residual stresses from shot peening and overload processes improve fatigue life of the system. In this work, experimental x-ray diffraction residual stress mapping was performed in the lugs of the unaffected portion of a 50 percent overloaded multi-lug breech ring that was fatigue tested to failure. Finite element modelling of a two-dimensional cross section of the breech block/ring assembly was performed using ABAQUS codes on a Convex C-220 computer. Comparisons of experimental residual stresses and finite element analysis (FEA) predictions showed good agreement in the major features of residual stress distribution, especially in the front lug. While FEA predicted the general characteristics of experimental residual stress distribution, experimental residual stresses were deeper and less compressive.				
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Multi-Lug Breech, Breech Mer Finite Element Analysis	chanism, Overload Process, EX3	5, Residual Stress,	15. NUMBER OF PAGES 21 16. PRICE CODE	
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are defined as piecewise conic "affine" refers to the fact that of numerical differentiation us system solved by Newton iteration are obtained based on conic splines is also it of the mathematical machinery applicable than global C ³ conipointwise sense. This apparer construction of the interpolant	s and are therefore guaranteed to we make no use of Euclidean disting conics. The nodal derivative ation—each iteration involving the by the aforementioned conic nuncluded, as well as a discussion of behind conic differentiation and ic splines are, as well as being cont increase of smoothness beyon	o be convex in the case of (stance or angle in the discusses for the conic splines satistic esolution of a pentadiagor americal differentiation. A f what we refer to as "sketch local C ³ conic splines. Sketcomputationally simpler, morald C ³ is obtained through a ce conics with or without re	envex) data point. These functions strictly) convex data. The modifier scion. We also include a discussion fly a locally quadrivariate quadratic that linear system. Initial values for discussion of numerical quadrature and interpolation, which makes use the interpolation is more generally the flexible, and smoother in a local process of re-sketching during the sketching. This is to say that if the at conic.
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Measurements of fracture toughnes	s were performed for seven weld a to of applied K to the critical K for	and heat-treat conditions of or fracture for various con	de based on available strain gage data. The 4130 steel used for the baseplate. Abinations of firing stress and material late were recommended.
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The world of interior ballistics has long clearly defined zero time point and no clearly peak pressure, but without a clear zero functions to establish a consistent time then be combined with the nominal peak	lear measure of the length of the o the time-to-peak is an elusiv reference zero time and a well-	pressure pulse. The normal be e concept. This work will de defined time-to-peak or time of	allistic plot usually has a rather clear emonstrate the use of mathematical
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or algorithms complete their work a B-spline which can be of arbitrar as desired. The algorithms auton one if desired. Part of the reason actually obtained or used explicit distribution function corresponding	in an amount of time proprily high smoothness. The smatically evaluate the smooth why this smoothing may be the control of the	noothed result or approximation over any edone so efficiently stem taturally to consideration es of a random variable—to on of a density, the use of	a over uniform meshes. These methods of data present. The kernel used here is mation may therefore also be as smooth a arbitrary mesh, including the original as from the fact that the kernel is never of smoothing the discrete cumulative a situation in which the original mesh is a positive kernel is important, because tives of the smooth approximation may
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There are several industrial processes w				
thickness undergoes plastic deformation, Autofrettage is a process whereby a thick				
while an outer sleeve remains elastic. Al				
stress distribution of the tubes under pres	sure and the corresponding pressure	e have to be determined in o	order to arrive a	t the retained stress distribution. In
general, when uniformly distributed radi	al stresses are acting on the outer	(diametrical) surface of a t	hick-walled mb	e, the tangential stress component
(throughout the tube's wall thickness) has surface of the same tube, the tangential	s the same sign as the radial compo	ment. If, however, uniformly	y distributed ra	dial stresses are acting on the inner
magnitude of the tangential stress compo				
surface, as well as with increasing magni	itude of the imposed radial stress. I	However, if loaded at the tu	be's interior aft	er plastic deformation commences,
the magnitude of the tangential compone	nt decreases (from a maximum at t	he elastic-plastic interface)	towards the tub	e's inner surface and in very large
wall thickness tubes it might reverse its si as that of the imposed radial component.				
of other related processes and/or product	s. A press-fitted concentric liner in	a thick-walled tube is such	an example.	Vhile the outer tube is subjected to
uniformly distributed radial stresses at it	s bore, the liner is subjected to the	same radial stresses at its	outer diameter.	During heat treatment of tubular
components, the cooled annulus imposes				
of the elastic-plastic interface diameter at the plastically deformed inner sleeve of				
responsible for such a distribution are als				
and isotropic and that Mises' yield criter				
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up to and above their respective glas	ss transition temperatures. Compo	site samples were subject	earbon/epoxy) was studied at temperatures eted to both short- and long-term heating. imples was cycled for 30-minute intervals
based on temperature and time at t	emperature. The results showed	good thermal stability for	ecorded. Weight loss data were compared or each epoxy material through its glass ong- and short-term temperature exposure.
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